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$$P = \frac{A_1 + a}{4A} - \frac{3a}{4} \sin \zeta - \frac{2a}{4} \sin \eta - \frac{a}{4} \sin \theta$$

$$p = \frac{A_1 + a}{4A} + \frac{1}{4} a \sin \zeta - \frac{1}{4} a \sin \eta - \frac{1}{4} a \sin \theta$$

$$r = \frac{A_1 + a}{4A} + \frac{1}{4} a \sin \zeta + \frac{1}{4} a \sin \eta - \frac{1}{4} a \sin \theta$$

$$s = \frac{A_1 + a}{4A} + \frac{1}{4} a \sin \zeta + \frac{3}{4} a \sin \eta + \frac{1}{4} a \sin \theta$$

atque

$$x = \frac{B_1 + b}{4A} - \frac{3}{4} a \cos \zeta - \frac{3}{4} a \cos \eta - \frac{1}{4} a \cos \theta$$

$$y = \frac{B_1 + b}{4A} + \frac{1}{4} a \cos \zeta - \frac{1}{4} a \cos \eta - a \cos \theta$$

$$z = \frac{B_1 + b}{4A} + \frac{1}{4} a \cos \zeta + \frac{1}{4} a \cos \eta - \frac{1}{4} a \cos \theta$$

$$v = \frac{B_1 + b}{4A} + \frac{1}{4} a \cos \zeta + \frac{3}{4} a \cos \eta + \frac{1}{4} a \cos \theta$$

concepit

cata PM

vero ma

ipius S,

 $\equiv dS \sin$ & A a \equiv $P = \frac{B_1 + b}{4A}$ $x = \frac{B_1 + b}{4A}$ si massam
sum praesi $Oa = \frac{B_1 + b}{4A}$ $Aa = \frac{B_1 + b}{4A}$ his integra
fs. Erit
Deinde cu
(A+B+C $- Aa \sin \zeta$
hac exprei $\Sigma (Oa + f)$
mili modostro casu tr
 $\sin \vartheta = \frac{a}{\cos \varphi} = \frac{a}{a}$

Problema. V.

32. Augatur nunc numerus corpusculorum in infinitum, filorum autem longitudines evanescent, ita ut hoc modo funis perfecte flexibilis formetur, cuius, si super piano horizontali utetur que projiciatur, motus & situs ad quodvis tempus assignari debet.

Solutio.

Pervenerit iste funis elapso tempore i infinitum A MG, ex cuius singulis punctis M perpendicula ad axem Oo demissa con-

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concipiantur. Vocetur abscissa quæcunque $OP = X$, applicata $PM = Y$, & longitudo portionis funis $AM = S$, ejus vero massa exprimatur per functionem quæmenique Σ ipsius S , sitque præterea angulus $AMP = \Phi$, ita ut sit $dX = dS \sin \Phi$ & $dY = dS \cos \Phi$. Ponatur ut ante $Oa = p$ & $Aa = x$, quia invenerimus

$$p = \frac{Aa + a + Aa \sin \zeta + (A + B)b \sin \eta + (A + B + C)c \sin \theta + \&c.}{A + B + C + E + \&c.}$$

$$x = \frac{Bt + b + Aa \cos \zeta + (A + B)b \cos \eta + (A + B + C)c \cos \theta + \&c.}{A + B + C + D + \&c.}$$

si massam totius funis ponamus $= H$, his formulæ ad casum præsentem translatis habebimus

$$Oa = \frac{Aa + a + \int \sum dS \sin \Phi}{H} - f dS \sin \Phi$$

$$Aa = \frac{Bt + b + \int \sum dS \cos \Phi}{H} - f dS \cos \Phi$$

His integralibus per totam funis longitudinem AMC extensis. Erit autem $f dS \sin \Phi = ag$ & $f dS \cos \Phi = Gg - Aa$. Deinde cum supra invenerimus: $Aa + Bq + Cr + Dr + \&c. = (A + B + C + D) + \&c.$ $(p + a \sin \zeta + b \sin \eta + c \sin \theta + \&c.) - Aa \sin \zeta - (A + B)b \sin \eta - (A + B + C)c \sin \theta - \&c.$ erit hæc expressio ad præsentem casum translata pro arcu $AM = \Sigma (Oa + f dS \sin \Phi) - \int \sum dS \sin \Phi = Oa \cdot \Sigma + f \int \Sigma f dS \sin \Phi$. Simili modo & altera expressio $Ax + By + Cz + Dr + \&c.$ nostro casu transit in hanc $Aa \cdot \Sigma + f \int \Sigma f dS \cos \Phi$; unde erit

$$\sin \Phi = \frac{dd(Oa \cdot \Sigma + f \int \Sigma f dS \sin \Phi)}{dd(Aa \cdot \Sigma + f \int \Sigma f dS \cos \Phi)}$$

$$\cos \Phi = \frac{dd(Aa \cdot \Sigma + f \int \Sigma f dS \cos \Phi)}{dd(Aa \cdot \Sigma + f \int \Sigma f dS \sin \Phi)}, \text{ quæ differentialia}$$

secundum-

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secundi gradus ex variabilitate temporis sola sunt defumenda, ita ut $S \& \Sigma$ tanquam constantia trahentur.

Quoniam ergo angulus Φ cum tempore t variatur, etiam si arcus S idem maneat, quantitas Φ erit functio duorum variabilium $S \& t$. Ponatur propterea $d\Phi = M dS + N dt$ eritque posito S constante & solo t variabilis.

$$d.Oa = \frac{M dt + d\int \Sigma N dS \cos \Phi}{H} - d\int N dS \cos \Phi$$

$$d.Aa = \frac{N dt - d\int \Sigma N dS \sin \Phi}{H} + d\int N dS \sin \Phi$$

Quia vero N est porro functio ipsarum $S \& t$ ponitur $dN = P dS + Q dt$, eritque posito solo t variabili, & dt constantes

$$dd.Oa = - \frac{d\int \Sigma N dS \sin \Phi + d\int \Sigma Q dS \cos \Phi}{H}$$

$$+ d\int N dS \sin \Phi - d\int Q dS \cos \Phi$$

$$dd.Aa = - \frac{d\int \Sigma N dS \cos \Phi - d\int \Sigma Q dS \sin \Phi}{H}$$

$$+ d\int N dS \cos \Phi + d\int Q dS \sin \Phi$$

quae singula integralia ad totam curvam erunt extendenda; ita ut ea abeant in functiones ipsius t tantum; hancobrem sit $dd.Oa = Edt$ & $dd.Aa = Fdt$, erunt E & F functiones ipsius t tantum. Deinde quae pertinent ad solum arcum indefinitum $\bar{A}M$, erunt differentialia, quae ex sola variabilitate ipsius t oriuntur:

 $d.f_2$ $d.f_1 / \sum f_1$ $dd.f_1 / d \sum f_1$ $d.f_1 / z f_1 S_1$ $d.d.f_1 / z f_1 S_1$ $Ex his erg$ $\frac{\sin \Phi}{\cos \Phi} =$ Qua $modius ex$ $Oa.z$ $Aa.z$ $fitque nob
ipsius & nat
um, quæ$ $Erit ergo$ f_1 anteced
& Aa const $Oa.d$ $Aa.d$ $& statuendi
& spectetur,$ $d \times dS$ $\rightarrow d \times dS$ $Euleri O_1$

$$d\int d\Sigma \int dS \sin \phi = d\int d\Sigma \int N dS \cos \phi$$

$$dd\int d\Sigma \int dS \sin \phi = - d\int d\Sigma \int N^2 dS \sin \phi + d\int d\Sigma \int Q dS \cos \phi,$$

$$d\int d\Sigma \int dS \cos \phi = - d\int d\Sigma \int N dS \sin \phi.$$

$$d\int d\Sigma \int dS \cos \phi = - d\int d\Sigma \int N^2 dS \cos \phi - d\int d\Sigma \int Q dS \sin \phi.$$

Ex his ergo obtinebitur sequens sequatio;

$$\frac{\sin \phi}{\cos \phi} = \frac{Ex - \int d\Sigma \int N^2 dS \sin \phi + \int d\Sigma \int Q dS \cos \phi}{Fx - \int d\Sigma \int N^2 dS \cos \phi - \int d\Sigma \int Q dS \sin \phi}$$

$$\frac{\sin \phi}{\cos \phi} = \frac{Ex - \int d\Sigma \int N^2 dS \cos \phi + \int d\Sigma \int Q dS \sin \phi}{Fx - \int d\Sigma \int N^2 dS \sin \phi - \int d\Sigma \int Q dS \cos \phi}$$

Quo autem naturam hujus curvæ ejusque motus commodius exprimamus, ponamus:

$$Oa. z + \int dz \int dS \sin \phi = T$$

$$Aa. z + \int dz \int dS \cos \phi = V$$

Itaque nobis & character differentialium, quæ ex variabilitate ipsius, nascuntur, manente & charactere differentialium tantum, quæ ex sola variabilitate ipsius S seu z ortum trahunt.

Erit ergo $\frac{\sin \phi}{\cos \phi} = \frac{\delta \delta T}{\delta \delta V}$: tum vero differentiendo formulæ antecedentes ponendo tantum z vel S variabili, ob Oa & Aa constantes erit

$$Oa. dz + \int dz \int dS \sin \phi = dT$$

$$Aa. dz + \int dz \int dS \cos \phi = dV$$

& statuendo d² constante, ita ut S tanquam functio ipsius z spectetur, si denuo differentialia sumantur, erit

$$dz \int dS \sin \phi = ddT$$

$$\Rightarrow dz \int dS \cos \phi = ddV$$

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ideoque $\frac{\sin \varphi}{\cos \varphi} = \frac{ddT}{ddV}$, unde obtinetur ista aequatio
 $\frac{\delta\delta T}{\delta\delta V} = \frac{ddT}{ddV}$

Præterea vero cum sit $\sin \varphi = \frac{ddT}{dxdS}$, & $\cos \varphi = \frac{ddV}{dxdS}$

debet esse $ddT + ddV = d^2 dS$. Quæstio ergo huc
redit ut investigentur duæ hujusmodi functiones ipsarum
 Σ & τ quæ sint T & V , ita ut earum differentialia secunda
posito solo Σ variabili cædem inter se teneant rationem,
quam cædem functionum differentialia secunda, si solum
 τ ponatur variabile: præterea vero debet esse $ddT +$
 $ddV = dS d\Sigma$: quibus inventis erit

$$\sin \varphi = \frac{ddT}{dS d\Sigma} \quad \& \cos \varphi = \frac{ddV}{dS d\Sigma}$$

Hincque porro coordinatae X & Y reperientur. Vel
cum sit $dX = dS \sin \varphi$ & $dY = dS \cos \varphi$, erit $ddT = d^2 dX$
& $ddV = d^2 dY$, unde sit $T = f/X d\Sigma$ & $V = f/Y d\Sigma$. Qua-
re X & Y ita comparatae esse debent, ut sit $\frac{\delta\delta T}{\delta\delta V} = \frac{dX}{dY}$
vel $\frac{f^2 \delta\delta X}{f^2 \delta\delta Y} = \frac{dX}{dY}$. Reducta ergo est solutio hujus pro-
blemati mechanici ad problema analyticum; in quo acqui-
scere oportet.

Q. E. J.

Scholion. I.

33. Quo hæc clarius explicentur, ponamus funem
ubique esse æque crassum, ita ut sit massa \propto proportionalis
longi-

longitudi
& longiti

Oa:

ubi integr
 $s = 0$, i
metur pei

Ase:

ubi integr
ut evanesc
 $s = h$.

Statuetur

$f ds$ si
 $f ds$ ci
 $f ds$ si
 $f ds$ ci

erit Oa

Ai

Dein
hic in P.
matur pro
spectetur,

$\frac{\sin \varphi}{\cos \varphi}$

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longitudini S. Sit portio AM \equiv S, angulus AMP $\equiv \theta$, & longitudo tota AMG $\equiv h$, eritque elapsus tempore t

$$Oa = At + a + \frac{\int s ds \sin \theta - h \int s ds \sin \theta}{h}$$

ubi integralia $\int s ds \sin \theta$ ita debent capi, ut evanescant posito $s \equiv 0$, tum vero statui oportet $s \equiv h$, sicque Oa exprimitur per functionem ipsius s. Simili modo erit

$$Aa = Bt + b + \frac{\int s ds \cos \theta - h \int s ds \cos \theta}{h}$$

ubi integralia $\int s ds \cos \theta$ & $\int s ds \cos \theta$ pariter ita accipi debent ut evanescant posito $s \equiv 0$, quo facto ubique faciendum est $s \equiv h$.

Statuetur brevitas ergo: fiatque casu $s \equiv h$

$\int s ds \sin \theta \equiv P$	$P \equiv A$
$\int s ds \cos \theta \equiv Q$	$Q \equiv B$
$\int s ds \sin \theta \equiv R$	$R \equiv C$
$\int s ds \cos \theta \equiv S$	$S \equiv D$

erit $Oa = At + a + \frac{C - Ah}{h};$

$$Aa = Bt + b + \frac{D - Bh}{h}$$

Deinde superior expressio generalis $\int dz / dS \cdot \sin \theta$ abit hic in $P \equiv$, & $\int dz / dS \cdot \cos \theta$ in $Q \equiv S$; ideoque si dsumatur pro charactere differentiationis, si s tantum variabile spectetur, erit

$$\frac{\sin \theta}{\cos \theta} = \frac{\delta \delta (C_s - Ah_s + Ph_s - Rh)}{\delta \delta (D_s - Bh_s + Qh_s - Sh)}$$

R 2

ubi

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ubi omisimus $\alpha + \beta$ & $\beta + \gamma$, quia horum differentialia secunda evanescunt. Quanquam autem hinc idoneæ functiones ipsarum & pro angulo & adhibendæ inveniri vix possunt, tamen ope harum valores, quos quis forte pro & exhibuerit, facile explorari possunt, utrum problemati satisfaciant necne.

Scholion. 2.

34. Quamvis zutem hoc problema sit difficillimum, si in genere consideretur, tamen unus extat casus specialis, quo solutu sit facillimum. Hic locum habet, si angulus & exprimatur per functionem ipsius & tantum, ita ut in eam tempus & non ingrediatur. Quia enim tum formulae $C_s - Ahs + Phs - Rh$ & $D_s - Bhs + Qhs - Sh$ a sola variabili & pendent, earum differentialia, quæ prodeunt, si solum & variable ponatur, evanescunt, siveque aequationi ultimæ satisfit. Hoc igitur casu funis instar corporis rigidi motu sibi parallelo feretur, ita ut singulæ ejus partes perpetuo ad axem Oo eandem inclinationem conservent, & singulorum punctorum M celeritates, tam secundum directionem axis Oo , quam axis ad eum normalis $O\omega$ inter se erunt aequales. Quare si funi initio hujusmodi motus fuerit impressus, ut primo saltē momento singula elementa ad axem Oo eandem inclinationem retineant, tum eodem motu perpetuo promoveri perget.

Coroll. 1.

35. Si ponatur $C_s - Ahs + Phs - Rh = T$ & $D_s - Bhs + Qhs - Sh = e$, erunt T & e ejusmodi functiones, quæ evanescunt tam si ponatur $s = 0$, quam si

$s = h$,
bent esse c

ddT :
in quibus
& ds consti
bet esse

ddT :
existente V

36.
possent, hal
tem omnes
in formulis
tut solutio
ratur.

37.
ponatur:
 $T =$
atque prob
casus $= o$ &
 N fiant $= C$

ddS :
Præterea V
 ddN
 ddN

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fit, $\equiv 4$. Ita autem praeterea istae functiones T & Θ debent esse comparatae, ut sit

$$ddT \equiv hds \sin \theta + dds \equiv hdi \cos \theta.$$

in quibus differentiationibus solum s possum est variabile & ds constans. Sin autem solum s variabile statuatur, debet esse

$$\delta\delta T \equiv Vdt \sin \theta \quad \& \quad \delta\delta \Theta \equiv Vdt \cos \theta$$

existente V functione quacunque.

Coroll. 2.

36. Si igitur hujusmodi functiones T & Θ inventari possent, haberetur solutio particularis problematis; sin autem omnes omnino functiones his proprietatibus gaudentes in formulis generalibus comprehendi possent, cum habetur solutio problematis generalis absoluta, qualis desideratur.

Coroll. 3.

37. Sint M & N & Θ functiones ipsorum s & t , & ponatur:

$T \equiv M \sin \theta - N \cos \theta$; $\Theta \equiv Mcos \theta - N \sin \theta$
atque problemati satisfiet, si primum T & Θ evanescant cum casu $s \equiv 0$ quam casu $s \equiv h$; quod fit, si his casibus M & N sint $\equiv 0$. Deinde vero requiritur ut sit

$$hds \equiv ddM - Md\theta - 2dNds - Ndd\theta$$

Praeterea vero debet esse

$$ddN - Nd\theta + Mds + 2dMds \equiv 0$$

$$\delta\delta N - N\delta\theta + M\delta ds + 2\delta Mds \equiv 0$$

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in quarum æquationum prima & secunda t & ds sunt constantia, in tertia vero s & ds constantia sunt posita.

Coroll. 4.

38. Ex æquationibus prima & secunda eliminando terminos continentes $d\phi^2$ obtinebitur hæc:

$$(M^2 + N^2)dd\phi + 2d\phi(MdM + NdN) = NddM - MddN - Nhds^2$$

ex cuius integratione eruitur

$$(M^2 + N^2)d\phi = NddM - MdM - hds/Nds$$

hincque porro $\phi = A \operatorname{tag} \frac{M}{N} - h \int \frac{ds/Nds}{M^2 + N^2}$. Qui valor

si in alterutra æquatione substituatur ponendo $\int Nds = K$ prodibit

$$MdM + NddN = hMds + \frac{hhK^2 ds}{M^2 + N^2} - \frac{(NdM - MdN)}{M^2 + N^2}$$

Addatur utrinque $dM^2 + dN^2$ & ponatur $M^2 + N^2 = v$ erit

$$vddv = \frac{hhK^2 ds}{v^2} + hMds = \frac{hhK^2 ds}{v^2} +$$

$$hds \sqrt{v - N}$$

ex qua si definitur v , ob K datum, per N , invenietur valor idoneus pro M substituendus. Tum vero N extertia æquatione determinari debet.

Co-

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Coroll. 5.

3o. Si sit $N = 0$, sequacio secunda statim dat $M^* ds = E ds$ & $ds = \frac{E ds}{M^*}$, qui valor in prima $h ds = ddM - M^* ds$ substitutus dabit, $h ds = ddM - \frac{E^* ds}{M^*}$. Statuitur $ds = v dM$, ut, ob ds constans sit $ddM = -\frac{ddM}{v}$, erit substitutione facta;

$$hv^* dM = -\frac{dv}{v} - \frac{E^* v^* dM}{M^*} \text{ seu}$$

$$hdM = -\frac{dv}{v^2} - \frac{E^* dM}{M^*}$$

cujus integrale est:

$$hM = \frac{1}{2v^2} + \frac{E^*}{2M^*} - F \text{ seu}$$

$$2hv^* M^* = M^* + E^* v^* - 2Fv^* M^* \text{ unde}$$

$$v^* = \frac{\pm M}{\sqrt{(2hM^* + 2FM^* - E^*)}}$$

$$\& r = \int \frac{\pm M^* M}{\sqrt{(2hM^* + 2FM^* - E^*)}}$$

Quoniam vero M debet evanescere posito tam $r = 0$ quam $r = h$, fiat $\frac{\pm M^* M}{\sqrt{(2hM^* + 2FM^* - E^*)}} = \pm G$ posito $M = 0$, atque G determinabitur per E , F & constantes.

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stantes. Fiat ergo $G = \frac{1}{2}h$, & conditiones requisitae implebuntur, si ponatur

$$s = \frac{1}{2}h \pm \sqrt{\frac{M^2 M}{V(2hM^2 + 2FM^2 - E^2)} - \frac{E^2 M}{M V(2hM^2 + 2FM^2 - E^2)}}$$

unde erit $d\theta = \pm \frac{EdM}{M V(2hM^2 + 2FM^2 - E^2)}$

ubi E & F erunt quantitates tum ex constantibus tum ex scompositae. Præterea vero si fieri potest, ita debent esse comparatae, ut etiam tertiae æquationi $M d\theta + 2s M d\theta = 0$ seu $M M d\theta = H dt$ satisfiat, quod fiet si $d\theta = \frac{H dt}{M M}$ fuerit integrabile: ejus enim integrale verum dabit angulum θ . Ubi notandum est, H designare functionem quamcunque ipsius s non involventem t , uti E est functio ipsius t non continens s . Hancobrem $\frac{Eds + Hdt}{MM}$ erit integrabile si fuerit $MM = EH$ in functionem quamplam quantitatis $\int \frac{ds}{H} + \int \frac{dt}{E}$, seu si sit $\frac{MM}{EH}$ functio hujus quantitatis $\int \frac{ds}{H} + \int \frac{dt}{E}$.

Problema. VI.

Fig. 9. 40. Conset corpus ABC duobus articulis AB & BC in B flexura invicem conjunctis, ita ut ambo circa B liberrime circumagi queant; queriturque motus, quo hoc corpus super piano, horizontali politissimo fit progressorum, postquam ipsi semel motus qualunque fuerit impressus.

So-

Euler

bus or
quovis
clapso
cujas
dicula
ticuli
bus pa
vocem

A
O

centri
amboru
uterque
Erit en
Celeriti
puncta

Celeriti

2 137 2

Solutio.

Suntis pro iubitu in piano horizontali duobus axi-
bus orthogonalibus $O\alpha$ & $O\omega$ sese decussantibus, ad quos
quovis momento posicio corporis referatur, pervenerit
et apso tempore quoconque t , corpus in statum ABC, ex
eius punctis A, B, C ad axem $O\alpha$ demittantur perpen-
dicula Aa , Bb , Cc . Sit porro K centrum gravitatis ar-
ticuli AB, & L centrum gravitatis articuli BG, ex qui-
bus pariter ad axem $O\alpha$ normales ducantur KP & LQ,
voventurque:

$$AK = a; BK = b; RL = \beta; LC = c;$$

$$OP = p; PK = z; OQ = q; QL = y;$$

$$\text{Ang. } AKP = \zeta; \text{ & ang. } BLQ = \eta.$$

ex quibus erit

$$q - p = b \sin \zeta + \beta \sin \eta \quad & y - x = b \cos \zeta + \beta \cos \eta.$$

Motus autem utriusque articuli, constat ex motu
centri gravitatis, quem resolvamus secundum directiones
amborum axium $O\alpha$ & $O\omega$, & ex motu rotatorio, quo
uterque articulas circa suum gravitatis centrum gyabitur.
Erit ergo

Celeritas puncti	secundum direc- tio- nem $O\alpha$	secundum direc- tio- nem $O\omega$
K	$= \frac{dp}{dt}$	$= \frac{dc}{dt}$
L	$= \frac{dq}{dt}$	$= \frac{dy}{dt}$

Celeritas rotatoria articuli AB circa centrum gravitatis K

$$\text{erit } = \frac{d\zeta}{dt} \text{ in distantia } = r.$$

Euleri Opercula Tom. III.

S

Celer.

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Celeritas rotatoria articuli BC circa centrum gravitatis L.

$$\text{erit } = \frac{d\eta}{dt} \text{ in distantia } = 1.$$

Nunc ad motum determinandum sit:

$$\text{massa articuli AB} = K; \text{ articuli BC} = L$$

$$\text{momentum inertiae articuli AB} = KI; \text{ articuli BC} = LI$$

Momenta haec inertiae respectu utriusque articuli centri gravitatis sumi ponuntur, estque momentum inertiae aggregatum omnium corporis particularum per quadrata distantiarum suarum ab axe, circa quem corpus mobile concipitur, multiplicatarum. His positis si ambo articuli a se invicem essent dissoluti, uterque eundem motum tam progressivum ceneri gravitatis quam rotatorium circa axem verticalem per centrum gravitatis transeuntem perpetuo conservaret. Quoniam autem junctura in B sunt colligati, ambo isti motus se mutuo continuo perturbabunt, haecque perturbationes provenient a vi, quam junctura in B sustinet. Quae vis cum sit incognita, ponamus ab ea articulum AB usque duabus viribus, altera in directione $B\dot{\theta}$ quae sit $= B$, altera in directione Bx quae sit $= B$; atque alter articulus EC iisdem viribus, at in directionibus oppositis urgetur, scilicet in directione $B/vi = R$ & in directione $B\lambda/vi = S$. His ergo viribus primum motus centri gravitatis afficietur, scilicet primo quidem vis $Bx = B$ accelerabit motum centri gravitatis K secundum $O\omega$, & vis $B\dot{\theta} = B$ motum in directione $O\omega$; contra vero vis $B\lambda = S$ retardabit motum centri gravitatis L secundum $O\omega$, & vis $B/vi = R$ motum in directione $O\omega$. Hinc ex legibus sollicitationum erit:

$$2Kddp = Bdt \cdot \frac{d}{dt}$$

$$2Kddx = Bde \cdot \frac{d}{dt}$$

$$2Lddq =$$

Porro momentum est $= B\beta$ accelerabitur, quae $= \zeta$: momentum rotatorium ad angulum sollicitationis

$$2Kdd$$

Deinde momentum L est $= B\beta$ BC accelerans $= B\beta \sin \eta$, de erit;

$$2Lidd$$

His sollicitationes patis inventae

$$Kddp + \frac{d}{dt}$$

und

$$Kp +$$

$$Kx -$$

Cum igitur $\frac{d}{dt} + \beta \cos \eta$

$$(K+L)$$

$$(K+L)$$

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$$2Lddq = -Bdt; \quad 2Lddy = -Bdt$$

Porro momentum vis $Bx = B$ respectu centri gravitatis K est $= Bb \cos \zeta$, eoque motus rotatorius articuli AB accelerabitur, quoniam id tendit ad augendum angulum ACP $= \zeta$: momentum autem vis $Bt = B$ erit $= Bb \sin \zeta$, eoque motus rotatorius articuli AB retardabitur, quoniam id tendit ad angulum ACP $= \zeta$ minuendum. Unde ex legibus sollicitationum erit:

$$2Kdd\zeta = Bbdt \cos \zeta - Bbdt \sin \zeta$$

Deinde momentum vis $B\lambda = B$ respectu centri gravitatis L est $= B\beta \cos \eta$, tenditque ad motum rotatorium articuli BC accelerandum, momentum autem vis $Bt = B$, quod est $= B\beta \sin \eta$, retardabit eundem motum rotatorium, unde erit;

$$2Ldd\eta = B\beta dt \cos \eta - B\beta dt \sin \eta.$$

His sollicitationibus ad calculum revocatis, priores sequentes pro motu progressivo utriusque centri-gravitatis inventae dabunt,

$$Kddp + Lddq = c \quad & \quad Kddx + Lddy = 0 \\ \text{unde integrando elicetur}$$

$$Kp + Lq = f + f$$

$$Kx + Ly = G + g$$

Cum igitur sit $q = p + b \sin \zeta + \beta \sin \eta$ & $y = x + b \cos \zeta + \beta \cos \eta$ erit:

$$(K+L)p = f + f - Lb \sin \zeta - L\beta \sin \eta$$

$$(K+L)x = G + g - Lb \cos \zeta - L\beta \cos \eta$$

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$$\ddot{\theta} = \frac{\ddot{\alpha} + f - L b \sin \zeta - L \beta \sin \eta}{K + L} \quad -(K+)$$

$$\ddot{\alpha} = \frac{\ddot{\theta} + g - L b \cos \zeta - L \beta \cos \eta}{K + L} \quad -(K+)$$

$$\text{Ideoque } \ddot{\alpha} p = -\frac{L b d d. \sin \zeta - L \beta d d. \sin \eta}{K + L} \quad \text{ex quib[us}$$

$$\ddot{\alpha} q = \frac{K b d d. \sin \zeta + K \beta d d. \sin \eta}{K + L} \quad -(K+)$$

$$\ddot{\alpha} r = \frac{L b d d. \cos \zeta - L \beta d d. \cos \eta}{K + L} \quad -(K+)$$

$$\ddot{\alpha} s = \frac{K b d d. \cos \zeta + K \beta d d. \cos \eta}{K + L} \quad -(K+)$$

Ergo hinc vires \mathfrak{B} & B ita definiuntur ut sit:

$$\mathfrak{B} dt^* = -\frac{2 K L}{K + L} (b d d. \sin \zeta + \beta d d. \sin \eta) \quad M_1$$

$$B dt^* = -\frac{2 K L}{K + L} (b d d. \cos \zeta + \beta d d. \cos \eta) \quad \text{et que pr}$$

Qui valores si in aequationibus ex sollicitationibus motus rotatorii utriusque articuli ortis substituantur, prodibit:

$$K k k d d \zeta^2 = -\frac{K L}{K + L} (+b b \cos^2 \alpha d d \sin^2 \alpha + b \beta \cos^2 \alpha d d \sin \alpha) \quad S i t \zeta^2 + 1$$

$$L l l d d \eta^2 = -\frac{K L}{K + L} (+b \beta \cos^2 \alpha d d \sin^2 \alpha + \beta \beta \cos^2 \alpha d d \sin \alpha) \quad e r i t :$$

Cum ergo sit $\cos m d d. \sin n - \sin m d d. \cos n = d d \cos(m-n) + d n \sin(m-n)$ habebuntur ita aequationes.

-(K)

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$$-\frac{(K+L)kkdd\zeta}{Lb} = bdd\zeta + \beta dd\eta \cos(\zeta - \eta) \\ + \beta d\eta \sin(\zeta - \eta)$$

$$-\frac{(K+L)lld\eta}{K\beta} = add\eta + bdd\zeta \cos(\zeta - \eta) \\ - bd\zeta \sin(\zeta - \eta)$$

ex quibus per integrationem elicuntur:

$$-\frac{(K+L)kkd\zeta}{Lb} = bdd\zeta + \beta dd\eta \cos(\zeta - \eta) \\ + \beta fdd\eta \sin(\zeta - \eta)$$

$$-\frac{(K+L)lld\eta}{K\beta} = add\eta + bd\zeta \cos(\zeta - \eta) \\ - bd\zeta \sin(\zeta - \eta)$$

Multiplicetur prior per b posterior per f & addantur,
atque prodibit:

$$-\frac{(K+L)kkd\zeta}{L} - \frac{(K+L)lld\eta}{K} = bdd\zeta + add\eta + b\alpha \\ (d\zeta + d\eta) \cos(\zeta - \eta) \equiv fdr\gamma f$$

$$\text{ita } \pm fdr\gamma f = \frac{(K+L)(Kkkd\zeta + Llld\eta)}{KL} + bdd\zeta + add\eta \\ + b\alpha(d\zeta + d\eta) \cos(\zeta - \eta)$$

$$\text{Sit } \zeta + \eta = r \text{ & } \zeta - \eta = s, \text{ ut } \zeta = \frac{r+s}{2} \text{ & } \eta = \frac{r-s}{2}$$

erit:

$$\pm fdr\gamma f = \frac{(K+L)kkdr}{2L} + \frac{(K+L)kkds}{2L} + b\alpha dr \cos s \\ + \frac{(K+L)lldr}{2K} - \frac{(K+L)llds}{2K}$$

S 3

+

$$\begin{aligned} & \textcircled{1} \quad \textcircled{2} \\ & + \frac{bbdv}{2} + \frac{bbdu}{2} \\ & + \frac{ppdv}{2} - \frac{ppdu}{2} \end{aligned}$$

Ponitur porro $\frac{fdt\sqrt{f}}{b_p} = \frac{dt}{\sqrt{f}}$ atque
 $\frac{(K+L)kk}{2Lb_p} + \frac{(K+L)ll}{2Kb_p} + \frac{b}{2p} + \frac{b}{2b} = m$

$$\frac{(K+L)kk}{2Lbc} - \frac{(K+L)ll}{2Kbc} + \frac{b}{2c} - \frac{c}{2b} = n \quad \text{erit.}$$

$$\frac{dt}{\sqrt{f}} = mdv + ndu + dv \cos u$$

superiores vero aequationes differentio-differentiales in hanc
formam transmutentur.

$$o = \frac{(K+L)kkdd\zeta}{Lbc} + \frac{b}{c} dd\zeta^2 + dd\eta \cos(\zeta^2 - \eta) + d\eta \sin(\zeta^2 - \eta)$$

$$o = \frac{(K+L)lldd\eta}{Kbc} + \frac{c}{b} dd\eta + dd\zeta \cos(\zeta^2 - \eta) - d\zeta \sin(\zeta^2 - \eta)$$

quae invicem suberadæ dabunt:

$$o = nddv + mddu - ddu \cos u + \frac{1}{2}(dv^2 + du^2) \sin u$$

Prior vero $\frac{dt}{\sqrt{f}} = mdv + ndu + dv \cos u$ suppedicit

$$dv = \frac{dt \cdot \sqrt{f} - ndv}{m + \cos u} \quad \& \quad ddu = \frac{-nddu}{m + \cos u} +$$

$$\frac{dt du \sin u: \sqrt{f} - ndu \sin u}{(m + \cos u)^2}$$

atque

$$\text{atque } \frac{1}{2} d\theta \sin u = \frac{\frac{1}{2} dt^2 \sin u : f - nddu \sin u : \sqrt{f + \frac{1}{4} n^2 du^2 \sin^2 u}}{(m + \cos u)^2}$$

quibus valoribus substitutis obtinebitur:

$$\begin{aligned} o &= \frac{mddu}{m + \cos u} + \frac{nnddu \sin u : \sqrt{f - nn^2 du^2 \sin^2 u}}{(m + \cos u)^2} \\ &\quad + \frac{mddu + \frac{1}{2} dt^2 \sin u : f - nddu \sin u : \sqrt{f + \frac{1}{4} n^2 du^2 \sin^2 u}}{(m + \cos u)^2} \\ &\quad - ddu \cos u \\ &\quad + \frac{\frac{1}{2} dt^2 \sin u : f - \frac{1}{4} n^2 du^2 \sin^2 u}{m + \cos u} \end{aligned}$$

quae reducitur ad hanc:

$$\begin{aligned} o &= (mm - nn) ddu - ddu \cos u + \frac{\frac{1}{2} dt^2 \sin u : f - \frac{1}{4} n^2 du^2 \sin^2 u}{m + \cos u} \\ &\quad + \frac{\frac{1}{2} mdu \sin u + \frac{1}{2} du \sin u \cos u}{m + \cos u} \end{aligned}$$

$$\begin{aligned} \text{ita } o &= 2(mm - nn) ddu - 2ddu \cos u + du \sin u \cos u \\ &\quad + \frac{dt^2 \sin u : f + (m^2 - n^2) du \sin u + mdu \sin u \cos u}{m + \cos u} \end{aligned}$$

$$\text{Sit } dt = \frac{du}{\sqrt{w}} \text{ erit } ddt = o = \frac{ddu}{\sqrt{w}} - \frac{d\cos u}{2w\sqrt{w}}, \text{ ideoque}$$

$$ddu = \frac{dw}{2w}, \text{ quibus valoribus pro } ddu \text{ & } dt \text{ substitu-} \\ \text{tis fieri}$$

$$\begin{aligned} o &= (mm - nn) \frac{dw}{w} - \frac{dw \cos u}{w} + du \sin u \cos u + \\ &\quad \frac{du \sin u : f w + (m^2 - n^2) du \sin u + mdu \sin u \cos u}{m + \cos u} \end{aligned}$$

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Sive

$$\frac{(mm - nn) \cos - \cos \sin u^2 + \omega \sin \sin u \cos u}{m + \cos u} + \\ \frac{\sin u : f + (m^2 - n^2) \cos \sin u + m \omega \sin u \cos u}{(m + \cos u)^2} = 0$$

cujus integrale est

$$\frac{(mm - nn) \cos}{m + \cos u} - \frac{\omega \cos u^2}{m + \cos u} + \frac{x}{f(m + \cos u)} = g.$$

hinc sit $\omega = \frac{f(m + \cos u) - g}{fg(mm - nn - \cos u)}$ atque

$$dt = \frac{du \sqrt{fg(mm - nn - \cos u^2)}}{\sqrt{(mf - g + f \cos u)}} \text{ quo invento habebitur}$$

$dv = \frac{dt: \sqrt{f - ndu}}{m + \cos u}$ sicque per unicam variabilem u determinabuntur t , v , porroque anguli ζ & η , quibus inventis reliquae quantitates p , q , x , & y innotescant, ex quibus non solum positio corporis, sed etiam ejus motus definitur. Q. E. J.

Coroll. I.

41. Ex aequationibus $Kddp + Lddq = 0$ & $Kddx + Lddy = 0$ intelligitur corporis ABC centrum gravitatis uniformiter in directum progredi.

Coroll. 2.

42. Eandem vero quoque vivarum quantitatem conservari, hoc modo patebit:

2K

$$\frac{du \sqrt{f}}{E}$$

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$$\frac{2Kdpddp}{dt^2} = \mathfrak{B}dp; \quad \frac{2Kdxddx}{dt^2} = Bdx$$

$$\frac{2Ldqddq}{dt^2} = -\mathfrak{B}dq; \quad \frac{2Kdyddy}{dt^2} = -Bdy$$

$$\text{Est vero } dp - dq = -bd \cdot \sin \zeta - cd \cdot \sin \eta$$

$$dx - dy = -bd \cdot \cos \zeta - cd \cdot \cos \eta$$

$$\text{Ergo } \frac{K(dp^2 + dx^2) + L(dq^2 + dy^2)}{dt^2} = -\mathfrak{B}(bd \cdot \sin \zeta + bd \cdot \sin \eta) - B(bd \cdot \cos \zeta + cd \cdot \cos \eta)$$

$$\text{Porro vero est } \frac{Kkdd\zeta^2}{dt^2} = \mathfrak{B}bd \cdot \sin \zeta + Bbd \cdot \cos \zeta \text{ atque}$$

$$\frac{Llld\eta^2}{dt^2} = \mathfrak{B}cd \cdot \sin \eta + Bcd \cdot \cos \eta; \text{ quibus in unam summam collectis erit.}$$

$$\frac{K(dp^2 + dx^2 + kkd\zeta^2) + L(dq^2 + dy^2 + lld\eta^2)}{dt^2} = \text{Constanti}$$

At vero ista expressio exhibit vim vivam totius corporis,

$$\text{nam } \frac{K(dp^2 + dx^2 + kkd\zeta^2)}{dt^2} \text{ est vis viva articuli A B; atque}$$

$$\frac{L(dq^2 + dy^2 + lld\eta^2)}{dt^2} \text{ est vis viva articuli B C.}$$

Scholion.

43. Cum generaliter æquatio ultimo inventa $dt = \frac{du \sqrt{f g (mm - nn - \cos u)}}{\sqrt{(mf - g + f \cos u)}}$ integrationem non admittat,

Euleri Opuscula Tom. III.

T

casus